

# AX 1 Full-wave gas-filled rectifying valve

The AX 1 is a full-wave gas-filled rectifying valve for use in the smaller class of amplifiers.

## FILAMENT RATINGS

Heating: direct, by A.C.  
 Filament voltage. . . . .  $V_f = 4.0$  V  
 Filament current. . . . .  $I_f = 2.4$  A

## MAXIMUM RATINGS

Secondary (A.C.) voltage of the power transformer on no load. . . . .  $V_{tr} = \text{max. } 2 \times 500$  V<sub>eff</sub>  
 D.C. output . . . . .  $I_o = \text{max. } 125$  mA  
 Voltage drop in the valve . . . . .  $V_{arc} = \text{max. } 15$  V  
 Capacitance of the capacitor across the input of the smoothing circuit . . . . .  $C = \text{max. } 64$   $\mu$ F  
 When a capacitor is connected across the input of the smoothing circuit:  
 The ohmic resistance in the D.C. circuit, with  $C = 64$   $\mu$ F . . . . .  $R_t = \text{min. } 200$  ohms  
 The ohmic resistance in the D.C. circuit, with  $C = 32$   $\mu$ F . . . . .  $R_t = \text{min. } 150$  ohms  
 The ohmic resistance in the D.C. circuit, with  $C = 10$   $\mu$ F . . . . .  $R_t = \text{min. } 100$  ohms

## KEY TO SYMBOLS

The ohmic resistance  $R_t$  in the D.C. circuit, when the smoothing circuit commences with a capacitor, constitutes the ohmic resistance of the secondary winding of the transformer together with that of the transformer primary, i.e.  $R_t = R_s + n^2 R_p$ . If the first component of the smoothing circuit is a choke, however, this resistance value must be augmented to the extent of the ohmic resistance of that choke:

$R_t = R_L + R_s + n^2 R_p$ . The voltage delivered may be calculated from the expression:  $V_o = 0.45 V_{tr} - I_o R_t - V_{arc}$ , in which  $V_{tr}$  is the effective alternating voltage of the secondary winding of the transformer, for example  $V_{tr} = 2 \times 500$  V. The inductance of the choke should be at least equal to  $\frac{R_a}{1,000}$  or  $\frac{V_o}{V_i}$  ( $V_o$  in volts and  $I_o$  in mA),

where  $I_o$  is taken to be the lowest value occurring; in an amplifier having two output valves in a balanced output stage, this will be the current flowing in the amplifier without excitation. From this it will be seen that with a 12-henry choke, the characteristics begin to flatten out only at  $I_o = 30$  mA approx. At lower current values the loading curves rise steeply, owing to the effect of the smoothing capacitor. A choke having a higher inductance will produce straight characteristics down to lower current values, for instances 42 henries — 10 mA.

Fig. 4 shows the loading characteristics of the AX 1 used in a circuit in which a capacitor is the first smoothing element, and comparison of these with the corresponding curves for a high vacuum valve such as the AZ 4 shows clearly that the former are

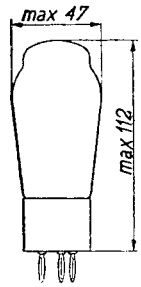


Fig. 1. Dimensions in mm.

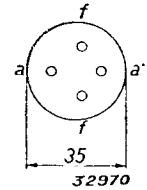


Fig. 2. Arrangement of electrodes and base connections

very much flatter with a low value of the internal resistance  $R_i$ ; also that the direct voltage is higher for the same alternating input. The direct voltages obtained from a smoothing circuit in which a capacitor is the first component are, further, higher than those in a circuit containing a choke as the first smoothing element.

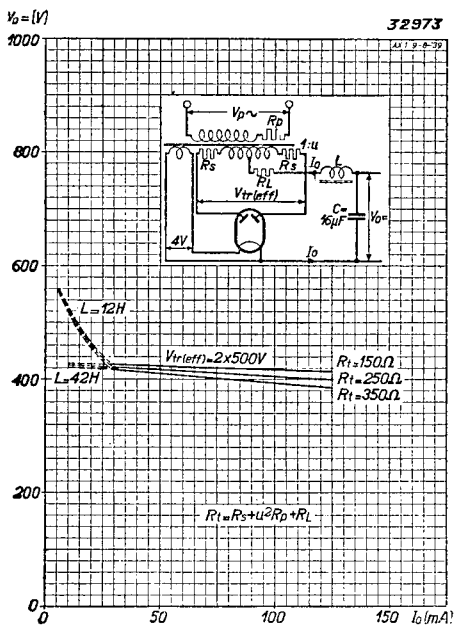


Fig. 3

Loading curves (D.C. voltage as a function of the current delivered) for various values of the resistance  $R_t = (R_L + R_s + n^2 R_p)$ , in a smoothing circuit commencing with a choke. The voltages at lower current values with a choke of 12 or 42 henries are shown by broken lines.

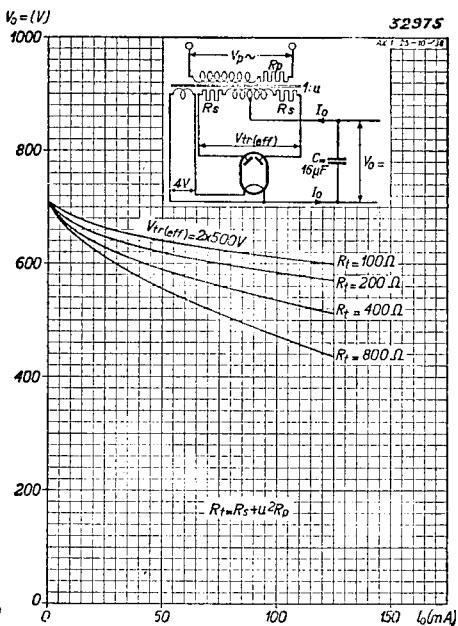


Fig. 4

Loading curves (D.C. voltage as a function of the delivered current) for various values of the total resistance  $R_t = (R_s + n^2 R_p)$ , in a smoothing circuit commencing with a capacitor.